Memoryless control of boundary concentrations of diffusing particles

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Flux between regions of different concentration occurs in nearly every device involving diffusion, whether an electrochemical cell, a bipolar transistor, or a protein channel in a biological membrane. Diffusion theory has calculated that flux since the time of Fick (1855), and the flux has been known to arise from the stochastic behavior of Brownian trajectories since the time of Einstein (1905), yet the mathematical description of the behavior of trajectories corresponding to different types of boundaries is not complete. We consider the trajectories of noninteracting particles diffusing in a finite region connecting two baths of fixed concentrations. Inside the region, the trajectories of diffusing particles are governed by the Langevin equation. To maintain average concentrations at the boundaries of the region at their values in the baths, a control mechanism is needed to set the boundary dynamics of the trajectories. Different control mechanisms are used in Langevin and Brownian simulations of such systems. We analyze models of controllers and derive equations for the time evolution and spatial distribution of particles inside the domain. Our analysis shows a distinct difference between the time evolution and the steady state concentrations. While the time evolution of the density is governed by an integral operator, the spatial distribution is governed by the familiar Fokker-Planck operator. The boundary conditions for the time dependent density depend on the model of the controller; however, this dependence disappears in the steady state, if the controller is of a renewal type. Renewal-type controllers, however, produce spurious boundary layers that can be catastrophic in simulations of charged particles, because even a tiny net charge can have global effects. The design of a nonrenewal controller that maintains concentrations of noninteracting particles without creating spurious boundary layers at the interface requires the solution of the time-dependent Fokker-Planck equation with absorption of outgoing trajectories and a source of ingoing trajectories on the boundary (the so called albedo problem).

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I. INTRODUCTION

We consider particles that diffuse between two regions where average concentrations are maintained at constant unequal values (see Fig. 1). Flux between regions of different concentration occurs in nearly every device involving diffusion, whether an electrochemical cell, a bipolar transistor, or a protein channel in a biological membrane. Continuum theories of such diffusive systems describe the concentration field by the (time independent) Nernst-Planck equation with fixed boundary concentrations [1–7].

The microscopic theory underlying diffusion describes motion of particles by Langevin's equations [3,5,8–10] everywhere, except at the boundaries. The behavior of the Langevin trajectories at the boundaries depends on the interaction between the particles and the boundaries. Thus, for example, outgoing trajectories can be terminated (absorbed);

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reflected (or otherwise reinjected); delayed; and so on. None of this is described by the Langevin equations. Brownian dynamics cannot describe such boundary behavior, because Brownian particles have no definite velocity, being functions of infinite variation. Particles with positive (e.g., incoming) velocities can be distinguished from those with negative (e.g., outgoing) velocities, only if their velocity is well defined [8]. The Langevin equations are often directly integrated in simulations [11–21].

In devices, the interaction between the trajectories and the boundaries must be specified because the inputs, outputs, and power supplies of devices are at their boundaries; in physical systems, the boundaries are where charge, matter, and energy are injected into a device; in biological systems boundaries represent reservoirs maintained at a (nearly) fixed electrochemical potential by active processes of the cell.

The formulation of boundary conditions for the particle concentration is obvious in macroscopic models, but formulation of boundary conditions for the underlying trajectories is not so clear cut, particularly because many different physical or computational control mechanisms can maintain a constant average density at prescribed locations, usually near the boundaries [11–15,19,22–28]. Many boundary conditions used in Brownian and Langevin simulations produce spuri-

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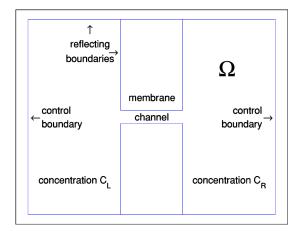


FIG. 1. The concentration cell of experimental electrochemistry and molecular biophysics. The region Ω typically consists of small parts of two large baths of effectively constant concentrations, separated by a permeable membrane in experimental electrochemistry, or (in biophysics) an impermeable membrane containing one or more channels.

ous boundary layers that do not exist at those locations in the physical systems being simulated. Spurious boundary layers are particularly damaging to simulations of charged particles. A boundary layer leads to large fluctuations in the electrostatic field which spreads over the entire simulation region. This was clearly demonstrated in Ref. [16] for a problem with equal boundary concentrations in a simulation with a buffer zone.

In this paper we provide a general description of the concentration and flux of noninteracting particles diffusing between constant average concentrations near the boundaries. We study renewal-type controllers that maintain fixed concentrations near the boundaries, determining the time course both of concentration (in phase space) and current. This kind of controllers is often used in simulations. We show that the concentration is a weighted sum of "left" and "right" concentrations, each of which satisfies a different integro-partialdifferential equation and different boundary conditions. In the steady state the phase space concentration is the weighted sum of the solutions of two stationary solutions of the so called *albedo* problem [29–34]. The albedo problem was first posed by Wang and Uhlenbeck [35] in 1945 and its analytic solution was first found by Marshall and Watson [36]. Further progress was made by Hagan, Doering, and Levermore [37,38], who used complex analysis to solve the half range expansion problem. The solution employed here was found by Kłosek [39]. The weights in the sum of "left" and "right" concentrations are the rates at which the controllers inject trajectories into the system.

Different control mechanisms that maintain the same concentrations near the boundaries produce different time operators that govern the evolution of the "left" and "right" concentrations. Each evolution is non-Markovian. The removal and injection—or re-injection—of particles into the system by renewal-type boundary controllers are described by renewal-type integral operators that govern the time evolutions of these concentrations, in contrast to the Fokker-Planck or Nernst-Planck equations that are commonly used.

The description of this simplified model of diffusion of noninteracting particles is apparently different: we include a detailed description of the physical mechanism that maintains the nonequilibrium state of the system. Similar descriptions are needed when particles interact.

II. FORMULATION

We consider a system composed of two finite macroscopic volumes containing electrolyte solutions of different ionic species, connected by a macroscopic or microscopic channel. A control mechanism keeps different average concentrations in the two volumes, so that a steady current flows through the system (see Fig. 1), thus keeping it out of equilibrium. As seen in the figure, the control mechanism is located only on parts of the boundaries of the system, at macroscopic distances away from the connecting channel. The control mechanism re-injects exiting trajectories at one or the other boundaries in a way that maintains average fixed concentrations near the boundaries at all times. We have in mind, for example, a typical setup used to measure the diffusion of ions through a protein channel of a biological cell membrane that separates two solutions of different fixed concentrations [1]. Alternatively, all trajectories are reflected at the boundary so that the system reaches equilibrium after a long time, but the long lasting transient regime is the nonequilibrium regime in which an almost steady current flows between the baths. This time behavior occurs when the number of particles that flow through the channel during the period of measurement is much smaller than the total number of ions in either bath.

The problem at hand is to describe the steady diffusion current flowing between the two baths, in terms of the molecular properties of the diffusing ions, such as their radii and interaction forces, as a function of the experimentally controlled variables, such as the concentrations in the two baths and the external potential, and as a function of the system geometry, e.g., the geometry and charge distribution of the channel.

The particles diffuse in a domain Ω that consists of the two macroscopic volumes and the connecting channel. We assume that there are N^h ions of species $h(h) = Ca^{++}, Na^+, Cl^-, \ldots$ in Ω , which are numbered at time t = 0, $\sum_h N^h = N$, and we follow their trajectories, $x_j^h(t) = (x_j^h(t), y_j^h(t), z_j^h(t))$ at all times t > 0 [$x_j^h(t)$ is the location of the jth ion of species h at time t].

For future use, the coordinate and velocity vectors of all ions in the 3*N*-dimensional configuration space, are denoted by $\tilde{x} = (x_1^{h_1}, \dots, x_{N^{h_1}}^{h_1}, x_1^{h_2}, \dots, x_{N^{h_2}}^{h_2}, \dots)$ and $\dot{\tilde{x}}$ or \tilde{v} .

Equations of motion

As in Ref. [5], we assume that the motion of an ion in the solution is overdamped diffusion in a field of force. The source of the noise and friction is the thermal motion of the solvent (e.g., water) and both are interrelated by Einstein's fluctuation-dissipation principle [3]. More specifically, our starting point is a memoryless system of *N* coupled Langevin

equations for the dynamics of all particles of the different species $h=Ca^{++}, Na^+, Cl^-, ...,$

$$\ddot{x}_{j}^{h} + \gamma^{h}(x_{j}^{h})\dot{x}_{j}^{h} = \frac{f_{j}^{h}(\widetilde{x})}{M^{h}} + \sqrt{\frac{2\gamma^{h}(x_{j}^{h})k_{B}T}{M^{h}}}\dot{w}_{j}^{h}, \quad (j = 1, 2, \dots, N^{h}),$$
(1)

where a dot on top of a variable means differentiation with respect to time, $\gamma^h(x^h)$ is the location dependent friction coefficient per unit mass, and M^h is the effective mass of an ion of species h. The force $f_j^h(\widetilde{x})$ on the jth ion of species h includes all ion-ion interactions and thus depends on the locations of all ions. The functions \dot{w}_j^h are, by assumption, independent standard Gaussian white noises. The parameter k_B is Boltzmann's constant and T is absolute temperature. As seen in Fig. 1, some parts of the boundary $\partial\Omega$ are reflecting, while other parts contain the control mechanism. At the boundary $\partial\Omega$, the random trajectories of the Langevin equations (1) are either reflected or are redirected by the external control mechanism.

III. RENEWAL CONTROLS

The solution of Eq. (1) depends on the specific choice of control mechanism. We first analyze controls for one-dimensional noninteracting systems because the treatment of three-dimensional interacting particle systems is more complicated. In this section we show that renewal controls (to be defined in Sec. III C) reproduce correct macroscopic properties such as total net flux and concentration profile, but also produce nonphysical boundary layers for noninteracting diffusive particle systems.

Consider particles diffusing in the interval $\Omega = [0,d]$. The control mechanism maintains average concentrations C_L and C_R at $0 \le x_L < x_R \le d$, respectively, *away* from the boundaries, where concentrations are actually measured. Each particle satisfies a Langevin equation

$$\ddot{x} + \gamma \dot{x} + U'(x) = \sqrt{2\gamma\epsilon} \dot{w}. \tag{2}$$

In order to complete the description of the dynamics we have to describe the motion of particles at the boundaries, i.e., to describe the action of the control mechanism.

A. Probabilistic control

A possible control mechanism operates as follows: when a particle reaches either one of the boundaries, it tosses a Bernoulli coin with probabilities (L,R), L+R=1, L, $R \ge 0$. The control mechanism decides to re-enter the particle at the left boundary x=0 with probability L, and to re-inject the particle to the bath at the right boundary x=d with probability R. The re-injections occur at random times; a particle that reached the boundary at time t, is delayed in the boundary a random time T and re-injected at time t+T. The random time T is a non-negative random variable with PDF,

$$q(s)ds = \text{Prob}\{s \le T < s + ds\}. \tag{3}$$

The velocity of injection is distributed according to predetermined distributions $s_L(v)$ and $s_R(v)$ of the left and right sources, respectively. For example, if both sources are Maxwellian, then

$$s_L(v) = \frac{2}{\sqrt{2\pi\epsilon}} e^{-v^2/2\epsilon} = s_R(-v), \quad v > 0.$$
 (4)

As shown below, the precise velocity distribution of the sources is unimportant for measurement of concentrations away from the boundaries.

The dynamics (1) and the boundary behavior provide a complete description of the trajectories, and therefore determine the probability distribution of the random particle trajectories in the system at any time. Assuming, as we may, that the precise velocity distribution is unimportant, there are only two parameters to be determined, namely, the fixed number of particles in the system N and the re-injection probability R. These two parameters determine uniquely the two measured concentrations C_L and C_R .

Let $p_i(x,v,t)$ be the probability of finding the ith particle at location x and velocity v at time t, given that it was injected to the bath at time t=0, from either the left or right boundary with probabilities R and L, and the corresponding velocity distributions s_L and s_R . Since the particles are independent and interchangeable, we find that $p_1=p_2=\cdots=p_N$, and set $p(x,v,t)=p_1(x,v,t)$. Let p(x,v) be the *steady state* density of a single particle, i.e., $p(x,v)=\lim_{t\to\infty}p(x,v,t)$. The steady state concentration at location x is given by

$$C(x) = N \int_{-\infty}^{\infty} p(x, v) dv.$$
 (5)

We use renewal theory [40] to calculate p(x,v). Suppose the device was turned on at time t=0. Let t_0 be the first time that the particle was injected into the system. Then the probability of finding the particle in location (x,v) of the phase space at time t is given by

$$p(x,v,t) = \int_0^t p(x,v,t|t_0 = s)q(s)ds.$$
 (6)

Let τ_1 be the first passage time of the particle to the boundary. Conditioning on τ_1 yields

$$p(x,v,t) = \int_0^t q(s)ds \int_0^\infty p(x,v,t|t_0 = s, \tau_1 = r)$$

$$\times p(\tau_1 = r|t_0 = s)dr,$$
(7)

where $p(\tau_1 = r | t_0 = s) = p(\tau = r - s) = 0$ for r < s. We separate the integral into two parts,

$$p(x,v,t) = \int_0^t q(s)ds \int_0^t p(x,v,t|t_0 = s, \tau_1 = r)p(\tau = r - s)dr$$

$$+ \int_0^t q(s)ds \int_t^\infty p(x,v,t|t_0 = s, \tau_1 = r)p(\tau = r - s)dr$$

$$= \int_0^t q(s)ds \int_0^t p(x,v,t-r)p(\tau = r - s)dr + f(x,v,t),$$
(8)

where

$$f(x,v,t) = \int_0^t q(s)ds \int_t^\infty p(x,v,t|t_0 = s, \tau_1 = r)p(\tau = r - s)dr.$$
(9)

Changing the order of integration in Eq. (8) we obtain

$$p(x,v,t) = \int_0^t p(x,v,t-r)dr \int_0^t q(s)p(\tau = r - s)ds + f(x,v,t)$$
$$= \int_0^t p(x,v,t-r)(p_\tau * q)(r)dr + f(x,v,t)$$
$$= (p * p_\tau * q)(t) + f(x,v,t), \tag{10}$$

where * denotes convolution. Taking the Laplace transform of the equation gives

$$\hat{p}(x,v,\theta) = \frac{\hat{f}(x,v,\theta)}{1 - \hat{p}_{\tau}(\theta)\hat{q}(\theta)}.$$
 (11)

The steady state distribution is given by

$$p(x,v) = \lim_{t \to \infty} p(x,v,t) = \lim_{\theta \to 0} \theta \hat{p}(x,v,\theta) = \lim_{\theta \to 0} \frac{\theta \hat{f}(x,v,\theta)}{1 - \hat{p}_{\tau}(\theta)\hat{q}(\theta)}.$$
(12)

Both numerator and denominator of the right hand side vanish as θ tends to 0. Expanding the denominator in Taylor series, we find that

$$p(x,v) = \frac{\hat{f}(x,v,\theta=0)}{\langle \tau \rangle + \langle T \rangle},\tag{13}$$

where $\langle \tau \rangle$ is the mean first passage time (MFPT), and $\langle T \rangle$ is the mean delay time before re-injection.

To evaluate $\hat{f}(x,v,\theta=0)$, we consider a Langevin particle in the interval [0,d] which is injected at time t=0 at x=0 with velocity distribution $s_L(v)$. When the particle reaches one of the boundaries, it is absorbed, and its trajectory is terminated at once. Let $\tilde{p}_L(x,v,t)$ be the probability density function of the particle (p) should not to be confused with \tilde{p}_L ; the subscript L stands for left). The density \tilde{p}_L satisfies the Fokker-Planck equation,

$$\frac{\partial \tilde{p}_L}{\partial t} = \mathcal{L}_{x,v} \tilde{p}_L = -v \frac{\partial \tilde{p}_L}{\partial x} + \frac{\partial}{\partial v} \{ [\gamma v + U'(x)] \tilde{p}_L \} + \epsilon \gamma \frac{\partial^2 \tilde{p}_L}{\partial v^2},$$
(14)

with the initial condition

$$\tilde{p}_L(x, v, t = 0) = \delta(x - 0^+) s_L(v),$$
(15)

and the absorbing boundary conditions

$$\tilde{p}_L(x=0^-,v,t)=0, \quad v>0,$$
 (16)

$$\tilde{p}_I(x = d, v, t) = 0, \quad v < 0.$$
 (17)

Equations (14)–(17) define the time dependent albedo problem. In the limit of high friction a new time scale is often used [10],

$$\hat{t} = t/\gamma, \tag{18}$$

so Eq. (14) is rewritten as

$$\frac{1}{\gamma} \frac{\partial \tilde{p}_L}{\partial \hat{t}} = \mathcal{L}_{x,v} \tilde{p}_L. \tag{19}$$

We define the function

$$P_L(x,v) = \int_0^\infty \tilde{p}_L(x,v,\hat{t})d\hat{t} = \frac{1}{\gamma} \int_0^\infty \tilde{p}_L(x,v,t)dt.$$
 (20)

The function $\gamma P_L(x,v)$ is the average time that a particle spends at location (x,v) prior to its absorption, given that it was injected from the left electrode at time t=0. It follows from Eqs. (14)–(17) that P_L , the solution of the steady state albedo problem, satisfies

$$\mathcal{L}_{x,v} P_L = -\frac{1}{\gamma} \delta(x - 0^+) s_L(v),$$
 (21)

with the absorbing boundary conditions

$$P_I(x=0^-,v)=0, \quad v>0,$$

$$P_I(x=d,v) = 0, \quad v < 0.$$
 (22)

The MFPT to the boundary $\langle \tau_L \rangle$ of a particle that was injected from the left electrode is given by

$$\langle \tau_L \rangle = \int_0^d \int_{-\infty}^{\infty} \gamma P_L(x, v) dx dv.$$
 (23)

Similarly, we define γP_R as the mean time spent by a trajectory at the point (x,v) prior to its absorption, given that it was injected to the bath from the right electrode at x=d at time t=0. The function P_R satisfies similar equations, and its integral is the MFPT $\langle \tau_R \rangle$.

Using the definition of f(x, v, t), Eq. (9), and changing the order of integration, we find that

$$\hat{f}(x,v,\theta=0) = \int_0^\infty f(x,v,t)dt$$

$$= \int_0^\infty dt \int_0^t q(s)ds$$

$$\times \int_t^\infty p(x,v,t|t_0=s,\tau_1=r)p(\tau=r-s)dr$$

$$= \int_0^\infty q(s)ds \int_s^\infty p(\tau=r-s)dr$$

$$\times \int_s^r p(x,v,t|t_0=s,\tau_1=r)dt. \tag{24}$$

We identify the inner two integrals as the mean total time that a particle had spent in the (x,v) location of phase space prior to its first absorption. Since $\int_0^\infty q(s)ds = 1$, we find that

$$\hat{f}(x,v,\theta=0) = L\gamma P_I(x,v) + R\gamma P_R(x,v), \qquad (25)$$

and

$$p(x,v) = \frac{L\gamma P_L(x,v) + R\gamma P_R(x,v)}{L\langle \tau_L \rangle + R\langle \tau_R \rangle + \langle T \rangle},$$
 (26)

from which the concentration in phase space is given by

$$C(x,v) = Np(x,v) = N\frac{L\gamma P_L(x,v) + R\gamma P_R(x,v)}{L\langle \tau_t \rangle + R\langle \tau_P \rangle + \langle T \rangle}.$$
 (27)

Equation (27) relates the probabilistic control mechanism to its resulting phase space steady state concentration, that satisfies the steady state Fokker-Planck equation with flux boundary conditions (21).

B. Rate control

Another possible renewal control consists of two sources, placed at the left and right boundaries, which inject particles into the system. When a particle reaches the right or left boundary, its trajectory is terminated at once. The sources inject particles at identical independent distributed (i.i.d.) interarrival random times T_L and T_R , whose probability density functions are $f_L(t)$ and $f_R(t)$, respectively. The rates of injection are defined as

$$\lambda_L = \frac{1}{\langle T_L \rangle}, \quad \lambda_R = \frac{1}{\langle T_R \rangle}.$$
 (28)

Note that the number of particles in the system does not remain fixed for this rate control mechanism. For any rectangle $A \subset [0,d] \times R$, we denote by $N_A^L(t)$ the number of particles in A at time t, that were originated at the left source. Then $N_A^L(t)$ satisfies a set of renewal equations [40],

$$\operatorname{Prob}\{N_{A}^{L}(t)=0\} = \operatorname{Prob}\{(x(t),v(t)) \in A\}$$

$$\times \left[\int_{0}^{t} f_{L}(s) \operatorname{Prob}\{N_{A}^{L}(t-s)=0\} ds + \int_{t}^{\infty} f_{L}(s) ds\right], \tag{29}$$

$$\begin{aligned} \operatorname{Prob}\{N_A^L(t) &= 1\} = \operatorname{Prob}\{(x(t), v(t)) \in A\} \\ &\times \left[\int_0^t f_L(s) \operatorname{Prob}\{N_A^L(t-s) = 0\} ds \right. \\ &+ \int_t^\infty f_L(s) ds \right] + \operatorname{Prob}\{(x(t), v(t)) \notin A\} \\ &\times \int_0^t f_L(s) \operatorname{Prob}\{N_A^L(t-s) = 1\} ds, \end{aligned} \tag{30}$$

$$\begin{split} \operatorname{Prob}\{N_A^L(t) = n\} &= \operatorname{Prob}\{(x(t), v(t)) \in A\} \\ &\times \int_0^t f_L(s) \operatorname{Prob}\{N_A^L(t-s) = n-1\} ds \\ &+ \operatorname{Prob}\{(x(t), v(t)) \notin A\} \\ &\times \int_0^t f_L(s) \operatorname{Prob}\{N_A^L(t-s) = n\} ds, \quad n > 1. \end{split} \tag{31}$$

Thus the expected value of $N_A^L(t)$ is given by

$$\langle N_A^L(t)\rangle = \sum_{n=1}^{\infty} n \operatorname{Prob}\{N_A^L(t) = n\} = \operatorname{Prob}\{(x(t), v(t)) \in A\}$$

$$\times \left[\int_0^t f_L(s) \langle N_A^L(t-s) \rangle ds + \int_0^{\infty} f_L(s) ds \right]$$

$$+ \operatorname{Prob}\{(x(t), v(t)) \notin A\} \cdot \int_0^t f_L(s) \langle N_A^L(t-s) \rangle ds$$

$$= \operatorname{Prob}\{(x(t), v(t)) \in A\} + \int_0^t f_L(s) \langle N_A^L(t-s) \rangle ds.$$
(32)

Dividing by the area |A| of A and taking the limit $|A| \rightarrow 0$, we obtain the number of particles per unit length and per unit velocity, which we call the phase space density $C^L(x, v, t)$. It satisfies the renewal equation

$$C^{L}(x,v,t) = \tilde{p}_{L}(x,v,t) + (f_{L} * C^{L})(x,v,t).$$
 (33)

Taking the Laplace transform with respect to t, we find that

$$\hat{C}^{L}(x,v,\theta) = \frac{\hat{\tilde{p}}_{L}(x,v,\theta)}{1 - \hat{f}_{I}(\theta)},$$
(34)

and the steady state density is given by

$$C^{L}(x,v) = \lim_{t \to \infty} C^{L}(x,v,t)$$

$$= \lim_{\theta \to 0} \frac{\theta \hat{\tilde{p}}_{L}(x,v,\theta)}{1 - \hat{f}_{L}(\theta)} = \frac{\hat{\tilde{p}}_{L}(x,v,0)}{\langle T_{L} \rangle}$$

$$= \lambda_{L} \hat{\tilde{p}}_{L}(x,v,0). \tag{35}$$

We obtain from Eq. (20) that

$$\hat{\tilde{p}}_L(x,v,0) = \int_0^\infty \tilde{p}_L(x,v,t)dt = \gamma P_L(x,v).$$
 (36)

The linearity of the expectation implies that the steady state concentration is

$$C(x,v) = C^{L}(x,v) + C^{R}(x,v) = \gamma \lambda_{L} P_{L}(x,v) + \gamma \lambda_{R} P_{R}(x,v).$$
(37)

C. Renewal control

Even though the two control models described above are different, and have different time evolution (e.g., the number of particles inside the domain is bounded by *N* for the former, and unbounded for the latter), they have *identical* steady state phase space concentrations. Indeed, choosing

$$\lambda_{L} = \frac{NL}{L\langle \tau_{L} \rangle + R\langle \tau_{R} \rangle + \langle T \rangle}, \quad \lambda_{R} = \frac{NR}{L\langle \tau_{L} \rangle + R\langle \tau_{R} \rangle + \langle T \rangle},$$
(38)

we find that Eqs. (27) and (37) are identical. This is no mere coincidence: both controls are special cases of renewal controls.

Definition 1. A source that injects particles into the domain at random times $0=T_0 \le T_1 \le T_2 ... \le T_n \le ...$, such that $Y_n=T_n-T_{n-1}$ are i.i.d. with $\langle Y_1 \rangle < \infty$ is called a renewal source

Definition 2. A control made of renewal sources located at the absorbing boundary of the domain is called a renewal control.

Theorem 1. The steady state phase space concentration of a renewal control is given by Eq. (37), where $\lambda_L = 1/\langle Y_1^L \rangle$, $\lambda_R = 1/\langle Y_1^R \rangle$ are the rates of the left and right renewal sources, respectively.

Proof. The proof is given in the previous subsection.

D. Calculation of P_L and P_R : The albedo problem

As seen above, all renewal control mechanisms require the knowledge of P_L and P_R , which are the solutions of the steady state albedo problem. It was shown in Ref. [39] that P_L is given by

$$P_L(x,v) = \frac{1}{\sqrt{2\pi\epsilon}} e^{-v^2/2\epsilon} e^{-U(x)/\epsilon} Q(x,v), \qquad (39)$$

where $Q = Q_{BL}^L + Q_{BL}^R + Q^{OUT}$, with $Q_{BL}^{L,R}$ the boundary layer solutions, which decay exponentially fast away from the boundaries, and Q^{OUT} the outer solution, given by

$$Q^{OUT}(x,v) = C \left[\int_0^x e^{U(z)/\epsilon} dz - \frac{1}{\gamma} v e^{U(x)/\epsilon} \right] + D + O(\gamma^{-2}), \tag{40}$$

with

$$C = \frac{e^{U(0)/\epsilon}}{\gamma \sqrt{\epsilon}} \frac{\zeta(\frac{1}{2}) + \mathcal{B}_0^L}{\int_0^d e^{U(z)/\epsilon} dz} + O(\gamma^{-2}),$$

$$D = -\frac{e^{U(0)/\epsilon}}{\gamma\sqrt{\epsilon}} \left[\zeta\left(\frac{1}{2}\right) + \mathcal{B}_0^L \right] + O(\gamma^{-2}), \tag{41}$$

where \mathcal{B}_0^L is a constant that depends on the velocity distribution of the left source, and ζ denotes the Riemann zeta function $\left[\zeta(\frac{1}{2}) = -1.460\ 035\ldots\right]$. The outer solution Q^{OUT} approximates Q at distances $O(\gamma^{-1})$ away from the boundaries. Similar expressions can be written for P_R .

E. Concentration profile and net flux

Equation (27) gives the concentration at x, which is established by the probabilistic control mechanism, as

$$C(x) = \frac{N\gamma [LP_L(x) + RP_R(x)]}{L\langle \tau_I \rangle + R\langle \tau_R \rangle + \langle T \rangle}.$$
 (42)

Therefore

$$\frac{C_L}{C_R} = \frac{LP_L(x_1) + RP_R(x_1)}{LP_L(x_2) + RP_R(x_2)}.$$
 (43)

We now solve Eq. (43) for the yet-undetermined parameter L that keeps constant concentrations C_L and C_R . Since L=1 -R, the solution is given by

$$L = \frac{C_R P_R(x_1) - C_L P_R(x_2)}{C_L [P_L(x_2) - P_R(x_2)] - C_R [P_L(x_1) - P_R(x_1)]}.$$
 (44)

Substituting in Eq. (42) we find that

$$\frac{N\gamma}{\langle \tau \rangle + \langle T \rangle} = \frac{C_L}{LP_L(x_1) + RP_R(x_1)},\tag{45}$$

and the two parameters of the control mechanism, N and L, are uniquely determined. We assume that the left and right sources have the same velocity density distribution, $s_L(v) = s_R(-v), v > 0$, which guarantees $\mathcal{B}_0^L = \mathcal{B}_0^R \equiv \mathcal{B}_0$. The resulting concentration at x away from the boundary is given by

C(x)

$$=\frac{C_{L}e^{[U(x_{1})-U(x)]/\epsilon}\int_{x}^{x_{2}}e^{U(z)/\epsilon}dz+C_{R}e^{[U(x_{2})-U(x)]/\epsilon}\int_{x_{1}}^{x}e^{U(z)/\epsilon}dz}{\int_{x_{1}}^{x_{2}}e^{U(z)/\epsilon}dz},$$
(46)

which is the same as given in Eq. (3.5) of Ref. [8]. Note that the constant factor $\zeta(\frac{1}{2}) + \mathcal{B}_0$ cancels out, and therefore it cannot be seen, if only concentrations are measured. The total net flux is given by

$$J(x) = N \int_{-\infty}^{\infty} v p(x, v) dv = \frac{N \gamma}{\langle \tau \rangle + \langle T \rangle} \int_{-\infty}^{\infty} v P(x, v) dv,$$
(47)

where $P = LP_L + RP_R$. The flux is constant and to leading order in γ^{-1} is given by

$$J = \frac{\epsilon}{\gamma} \frac{C_L e^{U(x_1)/\epsilon} - C_R e^{U(x_2)/\epsilon}}{\int_{x_1}^{x_2} e^{U(z)/\epsilon} dz}.$$
 (48)

We see that the macroscopic net flux (48) is $O(\gamma^{-1})$, and coincides with that given in Eq. (3.7) of Ref. [8] and in Ref. [1]. Theorem 1 then implies that Eqs. (46) and (48) describe the concentration and the flux for all renewal control mechanisms.

IV. DISCUSSION

The renewal controls studied here maintain systems of noninteracting particles at constant average concentrations near the boundaries, and away from the boundaries they produce the stationary Nernst-Planck equation of classical diffusion theory.

We have proven that all renewal controls produce the same steady state concentration and flux, even though their time evolutions can differ qualitatively. However, renewal controls—that are widely used in computer simulations—are problematic because they produce spurious boundary layers. These boundary layers are expected to appear in interacting particle systems driven out of equilibrium by renewal controls.

The existence of such boundary layers may be of little importance if the particles interact only through short range forces, such as Lennard-Jones forces, or the forces that prevent overlap of hard spheres. However, the boundary layers can have a catastrophic effect for particles that interact through long range forces, such as ions that interact electrostatically. The net charge carried by only a tiny fraction of the total number of ions is, after all, responsible for electrical signaling in the nervous system and the electrical potentials in electrochemical cells and these potentials extend over large distances, from micron to many meters, e.g., in the neurons of whales [41] as well as in inorganic applications from batteries to the trans-Atlantic cable [42–46].

The boundary behavior of diffusing particles has been studied for many types of boundaries, including absorbing, reflecting, sticky boundaries, and more [40,47]. In Ref. [22] a sequence of Markovian jump processes is constructed such that their transition probability densities converge to the solution of the Nernst-Planck equation with given boundary

conditions, including fixed concentrations and sticky boundaries.

As mentioned above, replacing the baths with renewal sources is a mathematical idealization that can produce artificial boundary effects. The renewal control effectively terminates trajectories at boundaries and starts new trajectories there. Most experiments do not. In real physical systems, particles that reach the boundary usually move into a "guard" region, from which they often return to the domain (with some probability), with a given time distribution. To capture this behavior by a mathematical model, the entire pdf of the first passage time for the albedo problem has to be found, not only its first moment. The spurious boundary layers will be avoided if the correct time course of recycling trajectories in and out of the domain is used. We postpone this calculation, which we could not find in the literature, to a future paper.

The time evolution of systems whose average concentrations near the boundaries are maintained by renewal controls is complicated and cannot be described, in general, by a single partial differential equation. We have shown that the phase space concentration is a sum of two components, each of which satisfies a different integral-partial-differential equation with different boundary conditions. Only in the steady state does the concentration satisfy the Fokker-Planck equation with boundary conditions identical to those of the steady state albedo problem. Although the overdamped limit is a useful approximation inside the domain, it cannot be used near the boundaries, where the full Fokker-Planck equation has to be solved. For particle systems with only short range interactions, the outer solution—which is the solution to the Smoluchowski equation-determines the concentration and correlation functions away from the boundaries. One can hope that a simple boundary condition can be found for such systems, similar to the simple boundary condition that exists for noninteracting systems.

From the theoretical point of view, the absence of a rigorous mathematical theory of the boundary behavior of Brownian trajectories diffusing between fixed concentrations, based on the physical theory of the Brownian motion, is a serious gap in classical physics. This paper is a step toward the bridging of this gap.

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